

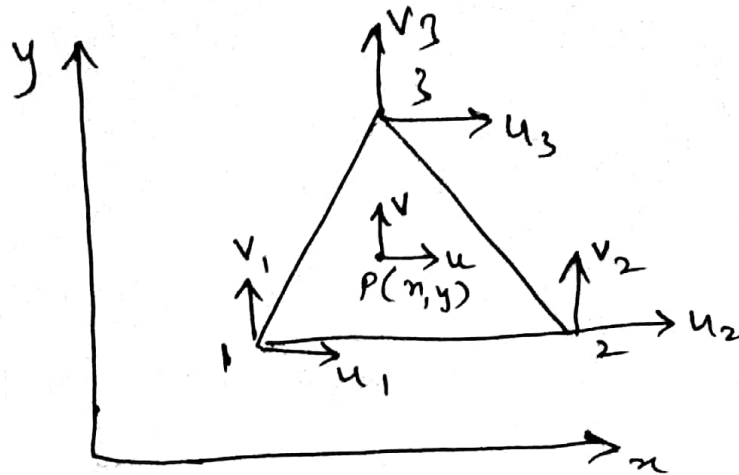
TWO DIMENSIONAL

SCALAR / VECTOR VARIABLE \Rightarrow

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UNIT-3

Derivation of Shape functions for Two dimensional Linear Element :



Consider CST element,

$\int \rightarrow$ displacement

$u \rightarrow$ displacement component in x axis

$v \rightarrow$ " " in y axis

$x, y \rightarrow$ Co-ordinates of nodes.

Polynomial eqn,

$$u(x, y) = a_1 + a_2 x + a_3 y$$

$$v(x, y) = a_4 + a_5 x + a_6 y.$$

apply nodal conditions,

$$u = u_1, \quad v = v_1, \quad x = x_1, \quad y = y_1,$$

$$u = u_2, \quad v = v_2, \quad x = x_2, \quad y = y_2$$

$$u = u_3, \quad v = v_3, \quad x = x_3, \quad y = y_3$$

So,

$$u_1 = a_1 + a_2 x_1 + a_3 y_1$$

$$u_2 = a_1 + a_2 x_2 + a_3 y_2$$

$$u_3 = a_1 + a_2 x_3 + a_3 y_3$$

&

$$v_1 = a_4 + a_5 x_1 + a_6 y_1$$

$$v_2 = a_4 + a_5 x_2 + a_6 y_2$$

$$v_3 = a_4 + a_5 x_3 + a_6 y_3$$

in matrix,

$$\begin{bmatrix} u_1 \\ u_2 \\ u_3 \end{bmatrix} = \begin{bmatrix} 1 & x_1 & y_1 \\ 1 & x_2 & y_2 \\ 1 & x_3 & y_3 \end{bmatrix} \begin{bmatrix} a_1 \\ a_2 \\ a_3 \end{bmatrix}$$

$$\begin{bmatrix} a_1 \\ a_2 \\ a_3 \end{bmatrix} = \begin{bmatrix} 1 & x_1 & y_1 \\ 1 & x_2 & y_2 \\ 1 & x_3 & y_3 \end{bmatrix}^{-1} \begin{bmatrix} u_1 \\ u_2 \\ u_3 \end{bmatrix}$$

(or)

$$[a] = [D^{-1}] [u]$$

$[D] \rightarrow$ Co-ordinate matrix

$$D^{-1} = \frac{C^T}{|D|}$$

$$[c] = \begin{bmatrix} c_{11} & c_{12} & c_{13} \\ c_{21} & c_{22} & c_{23} \\ c_{31} & c_{32} & c_{33} \end{bmatrix}$$

↳ Co-factor matrix

$$c_{ij} = (-1)^{i+j} \cdot |D_{ij}|$$

↳ minor matrix

$$c_{11} = (-1)^{1+1} \begin{vmatrix} x_2 & y_2 \\ x_3 & y_3 \end{vmatrix} = x_2 y_3 - x_3 y_2$$

Similarly calculate for all co-factors.

$$[c] = \begin{bmatrix} x_2 y_3 - x_3 y_2 & y_2 - y_3 & x_3 - x_2 \\ x_3 y_1 - x_1 y_3 & y_3 - y_1 & x_1 - x_3 \\ x_1 y_2 - x_2 y_1 & y_1 - y_2 & x_2 - x_1 \end{bmatrix}$$

$$[c]^T = \begin{bmatrix} x_2 y_3 - x_3 y_2 & x_3 y_1 - x_1 y_3 & x_1 y_2 - x_2 y_1 \\ y_2 - y_3 & y_3 - y_1 & y_1 - y_2 \\ x_3 - x_2 & x_1 - x_3 & x_2 - x_1 \end{bmatrix}$$

$$|D| = \begin{vmatrix} 1 & x_1 & y_1 \\ 1 & x_2 & y_2 \\ 1 & x_3 & y_3 \end{vmatrix}$$

$$|D| = 2A \quad [\text{Triangular area}]$$

$$\therefore [a] = [D^{-1}] [u]$$

$$\begin{bmatrix} a_1 \\ a_2 \\ a_3 \end{bmatrix} = \frac{1}{2A} \begin{bmatrix} x_2 y_3 - x_3 y_2 & x_3 y_1 - x_1 y_3 & x_1 y_2 - x_2 y_1 \\ y_2 - y_3 & y_3 - y_1 & y_1 - y_2 \\ x_3 - x_2 & x_1 - x_3 & x_2 - x_1 \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \\ u_3 \end{bmatrix}$$

$$= \frac{1}{2A} \begin{bmatrix} d_1 & d_2 & d_3 \\ \beta_1 & \beta_2 & \beta_3 \\ \gamma_1 & \gamma_2 & \gamma_3 \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \\ u_3 \end{bmatrix}$$

where,

$$d_1 = x_2 y_3 - x_3 y_2$$

$$d_2 = x_3 y_1 - x_1 y_3$$

$$d_3 = x_1 y_2 - x_2 y_1$$

$$\beta_1 = y_2 - y_3$$

$$\beta_2 = y_3 - y_1$$

$$\beta_3 = y_1 - y_2$$

$$\gamma_1 = x_3 - x_2$$

$$\gamma_2 = x_1 - x_3$$

$$\gamma_3 = x_2 - x_1$$

$$\therefore u(x, y) = \begin{bmatrix} 1 & x & y \end{bmatrix} \begin{bmatrix} a_1 \\ a_2 \\ a_3 \end{bmatrix}$$

$$u(x, y) = \begin{bmatrix} 1 & x & y \end{bmatrix} \frac{1}{2A} \begin{bmatrix} \alpha_1 & \alpha_2 & \alpha_3 \\ \beta_1 & \beta_2 & \beta_3 \\ \gamma_1 & \gamma_2 & \gamma_3 \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \\ u_3 \end{bmatrix}$$

$$= \frac{1}{2A} \begin{bmatrix} \alpha_1 + \beta_1 x + \gamma_1 y & \alpha_2 + \beta_2 x + \gamma_2 y & \alpha_3 + \beta_3 x + \gamma_3 y \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \\ u_3 \end{bmatrix}$$

$$= \begin{bmatrix} N_1 & N_2 & N_3 \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \\ u_3 \end{bmatrix}$$

$$u(x, y) = N_1 u_1 + N_2 u_2 + N_3 u_3$$

where,

$$N_1 = \frac{\alpha_1 + \beta_1 x + \gamma_1 y}{2A}$$

$$N_2 = \frac{\alpha_2 + \beta_2 x + \gamma_2 y}{2A}$$

$$N_3 = \frac{\alpha_3 + \beta_3 x + \gamma_3 y}{2A}$$

Similarly for, $v(x, y)$,

$$v(x, y) = N_1 v_1 + N_2 v_2 + N_3 v_3$$

finally,

displacement,

$$f(x, y) = \begin{bmatrix} u \\ v \end{bmatrix} = \begin{bmatrix} N_1 & 0 & N_2 & 0 & N_3 & 0 \\ 0 & N_1 & 0 & N_2 & 0 & N_3 \end{bmatrix} \begin{bmatrix} u_1 \\ v_1 \\ u_2 \\ v_2 \\ u_3 \\ v_3 \end{bmatrix}$$

$$f(x, y) = [N] \{f\}$$

Note:

$$N_1 + N_2 + N_3 = 1$$

Formulae :

* Stress - Strain relation,

$$[\sigma] = [D] [e]$$

$$\begin{bmatrix} \sigma_x \\ \sigma_y \\ \tau_{xy} \end{bmatrix} = [D] \begin{bmatrix} e_x \\ e_y \\ \gamma_{xy} \end{bmatrix}$$

$$D = \left[\frac{E}{1-\mu^2} \right] \begin{bmatrix} 1 & \mu & 0 \\ \mu & 1 & 0 \\ 0 & 0 & \frac{1-\mu}{2} \end{bmatrix} \text{ (plane stress)}$$

$$D = \frac{E}{(1+\mu)(1-2\mu)} \begin{bmatrix} 1-\mu & \mu & 0 \\ \mu & 1-\mu & 0 \\ 0 & 0 & \frac{1-2\mu}{2} \end{bmatrix} \text{ (plane strain)}$$

$\mu \rightarrow$ poisson ratio

$E \rightarrow$ young's modulus

$\sigma_x \rightarrow$ stress in x axis

$\sigma_y \rightarrow$ " in y axis

$\tau_{xy} \rightarrow$ shear stress

$e \rightarrow$ strain

* Strain - displacement relation

$$\{e\} = [B] \{f\}$$

$$[B] = \frac{1}{2A} \begin{bmatrix} \beta_1 & 0 & \beta_2 & 0 & \beta_3 & 0 \\ 0 & \gamma_1 & 0 & \gamma_2 & 0 & \gamma_3 \\ \gamma_1 & \beta_1 & \gamma_2 & \beta_2 & \gamma_3 & \beta_3 \end{bmatrix}$$

$$\{f\} = \begin{bmatrix} u_1 \\ v_1 \\ u_2 \\ v_2 \\ u_3 \\ v_3 \end{bmatrix}$$

$$e = \begin{bmatrix} e_x \\ e_y \\ \gamma_{xy} \end{bmatrix}$$

* Stress - displacement relation

$$[\sigma] = [D] [e]$$

$$[\sigma] = [D] [B] \{f\}$$

Maximum normal stress,

$$\sigma_1 = \frac{1}{2} \left[(\sigma_x + \sigma_y) + \sqrt{(\sigma_x - \sigma_y)^2 + 4\tau_{xy}^2} \right]$$

Minimum normal stress,

$$\sigma_2 = \frac{1}{2} \left[(\sigma_x + \sigma_y) - \sqrt{(\sigma_x - \sigma_y)^2 + 4\tau_{xy}^2} \right]$$

Maximum Shear Stress,

$$\tau_{\max} = \frac{1}{2} (\sigma_1 - \sigma_2)$$

Principle angle θ_p ,

$$\tan 2\theta_p = \frac{2\tau_{xy}}{\sigma_x - \sigma_y}$$

* Stiffness Matrix [K]

$$[K] = [B]^T [D] [B] A \cdot t$$

$$A = \frac{1}{2} \begin{vmatrix} 1 & x_1 & y_1 \\ 1 & x_2 & y_2 \\ 1 & x_3 & y_3 \end{vmatrix}$$

$t \rightarrow$ Thickness of element.

* Temperature effects:

$$e_0 = \begin{bmatrix} e_x \\ e_y \\ \gamma_{xy} \end{bmatrix} = \begin{bmatrix} \alpha \Delta T \\ \alpha \Delta T \\ 0 \end{bmatrix} \text{ (plane stress)}$$

$$e_0 = (1 + \mu) \begin{bmatrix} \alpha \Delta T \\ \alpha \Delta T \\ 0 \end{bmatrix} \text{ (plane strain)}$$

$d \rightarrow$ Thermal expansion Co-efficient

$\Delta T \rightarrow$ change in temperature.

$$[F_0] = [B]^T [D] [e_0] A \cdot t.$$

$$(6 \times 1) = (6 \times 3) (3 \times 3) (3 \times 1)$$

$$(6 \times 1) = (6 \times 1)$$

$$F_0 = \begin{bmatrix} F_{1x} \\ F_{1y} \\ F_{2x} \\ F_{2y} \\ F_{3x} \\ F_{3y} \end{bmatrix}$$

Note:

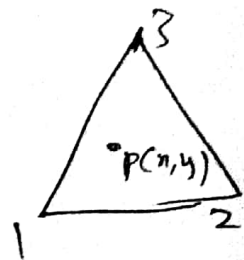
$$[F] = B^T D e_0 A t$$
$$= B^T D B \delta A t$$
$$[F] = [K] \cdot [\delta]$$

Isoparametric Representation:

WKT,

$$u = N_1 u_1 + N_2 u_2 + N_3 u_3$$

$$v = N_1 v_1 + N_2 v_2 + N_3 v_3.$$



Coordinates of point P,

$$x = N_1 x_1 + N_2 x_2 + N_3 x_3$$

$$y = N_1 y_1 + N_2 y_2 + N_3 y_3.$$

$$(N_1 + N_2 + N_3 = 1), \quad N_3 = 1 - N_1 - N_2.$$

Substitute,

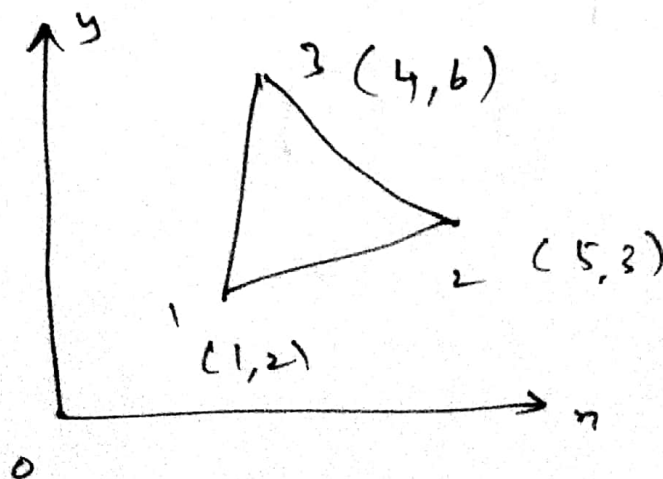
$$x = N_1 x_1 + N_2 x_2 + (1 - N_1 - N_2) x_3$$

$$x = (x_1 - x_3) N_1 + (x_2 - x_3) N_2 + x_3$$

Similarly,

$$y = (y_1 - y_3) N_1 + (y_2 - y_3) N_2 + y_3$$

- ① The nodal co-ordinates of a triangular element are shown in fig. At the point P inside the element, the x co-ordinate is 3.3 and the shape function $N_1 = 0.3$. Determine the shape functions N_2 , N_3 & y co-ordinate of the point P.



Sol:

$$x_1 = 1 \quad y_1 = 2$$

$$x_2 = 5 \quad y_2 = 3$$

$$x_3 = 4 \quad y_3 = 6$$

WCT,

$$x = (x_1 - x_3)N_1 + (x_2 - x_3)N_2 + N_3$$

$$3.2 = (1 - 4)0.3 + (5 - 4)N_2 + 4$$

$$N_2 = 0.2$$

$$N_1 + N_2 + N_3 = 1$$

$$0.3 + 0.2 + N_3 = 1$$

$$N_3 = 0.5$$

Then,

$$y = N_1 y_1 + N_2 y_2 + N_3 y_3$$

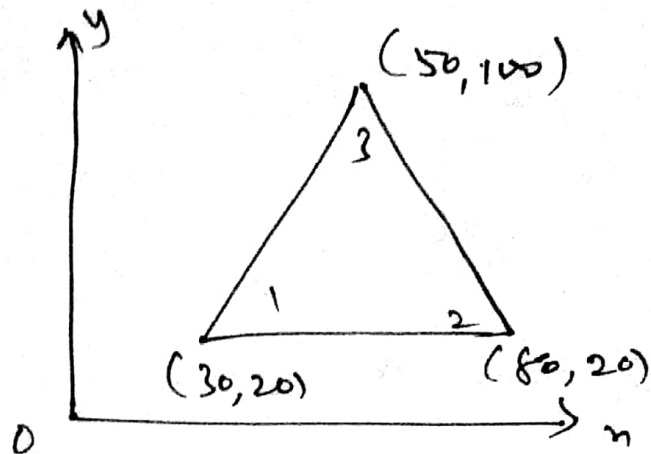
$$y = 0.3(2) + 0.2(3) + 0.5(6)$$

$$y = 4.2$$

② For the plane stress element shown in fig. evaluate the stiffness matrix. Assume

$$E = 210 \times 10^3 \text{ N/mm}^2, \quad \mu = 0.25, \quad t = 10 \text{ mm.}$$

The co-ordinates are given in mm.



Sol:

$$x_1 = 30$$

$$y_1 = 20$$

$$x_2 = 80$$

$$y_2 = 20$$

$$x_3 = 50$$

$$y_3 = 100$$

for CST,

$$[K] = [B]^T [D] [B] A t.$$

$$A = \frac{1}{2} \begin{vmatrix} x & x_1 & y_1 \\ 1 & x_2 & y_2 \\ 1 & x_3 & y_3 \end{vmatrix}$$

$$= \frac{1}{2} \begin{vmatrix} 1 & 30 & 20 \\ 1 & 80 & 20 \\ 1 & 50 & 100 \end{vmatrix}$$

$$A = 2000 \text{ mm}^2$$

$$[B] = \frac{1}{2A} \begin{bmatrix} \beta_1 & 0 & \beta_2 & 0 & \beta_3 & 0 \\ 0 & \gamma_1 & 0 & \gamma_2 & 0 & \gamma_3 \\ \gamma_1 & \beta_1 & \gamma_2 & \beta_2 & \gamma_3 & \beta_3 \end{bmatrix}$$

$$\beta_1 = y_2 - y_3 = 20 - 100 = -80$$

$$\beta_2 = y_3 - y_1 = 100 - 20 = 80$$

$$\beta_3 = y_1 - y_2 = 20 - 20 = 0$$

$$\gamma_1 = x_3 - x_2 = 50 - 80 = -30$$

$$\gamma_2 = x_1 - x_3 = 30 - 50 = -20$$

$$\gamma_3 = x_2 - x_1 = 80 - 30 = 50$$

$$\therefore [B] = \frac{1}{2 \times 2000} \begin{bmatrix} -80 & 0 & 80 & 0 & 0 & 0 \\ 0 & -30 & 0 & -20 & 0 & 50 \\ -30 & -80 & -20 & 80 & 50 & 0 \end{bmatrix}$$

$$= \frac{1}{4000} \begin{bmatrix} -8 & 0 & 8 & 0 & 0 & 0 \\ 0 & -3 & 0 & -2 & 0 & 5 \\ -3 & -8 & -2 & 8 & 5 & 0 \end{bmatrix}$$

$$[B]^T = \frac{1}{40} \begin{bmatrix} -8 & 0 & -3 \\ 0 & -3 & -8 \\ 8 & 0 & -2 \\ 0 & -2 & 8 \\ 0 & 0 & 5 \\ 0 & 5 & 0 \end{bmatrix}$$

for plane stress condition,

$$D = \frac{E}{1-\mu^2} \begin{bmatrix} 1 & \mu & 0 \\ \mu & 1 & 0 \\ 0 & 0 & \frac{1-\mu}{2} \end{bmatrix}$$

$$= \frac{210 \times 10^3}{1-0.25^2} \begin{bmatrix} 1 & 0.25 & 0 \\ 0.25 & 1 & 0 \\ 0 & 0 & \frac{1-0.25}{2} \end{bmatrix}$$

$$[D] = 56 \times 10^3 \begin{bmatrix} 4 & 1 & 0 \\ 1 & 4 & 0 \\ 0 & 0 & 1.5 \end{bmatrix}$$

finally,

$$[K] = \frac{1}{40} \begin{bmatrix} -8 & 0 & -3 \\ 0 & -3 & -8 \\ 8 & 0 & -2 \\ 0 & -2 & 8 \\ 0 & 0 & 5 \\ 0 & 5 & 0 \end{bmatrix} 56 \times 10^3 \begin{bmatrix} 4 & 1 & 0 \\ 1 & 4 & 0 \\ 0 & 0 & 1.5 \end{bmatrix} \times$$

$$\frac{1}{400} \begin{pmatrix} -8 & 0 & 8 & 0 & 0 & 0 \\ 0 & -3 & 0 & -2 & 0 & 5 \\ -3 & -8 & -2 & 8 & 5 & 0 \end{pmatrix} \quad 2000 \times 10.$$

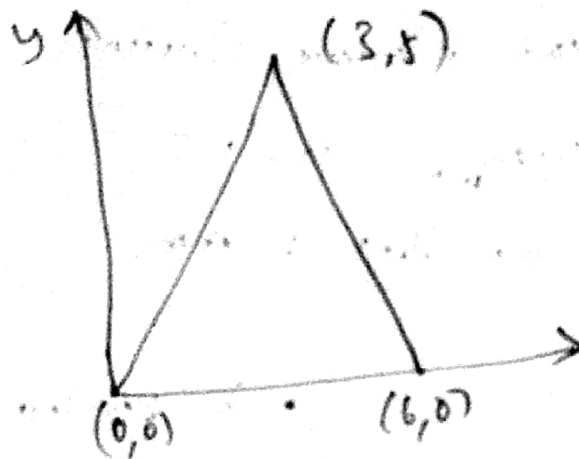
$$K = 7 \times 10^3 \begin{bmatrix} 269.5 & 60 & -247 & -20 & -22.5 & -40 \\ 60 & 132 & 0 & -72 & -60 & -60 \\ -247 & 0 & 262 & -40 & -15 & 40 \\ -20 & -72 & -40 & 112 & 60 & -40 \\ -22.5 & -60 & -15 & 60 & 37.5 & 0 \\ -40 & -60 & 40 & -40 & 0 & 100 \end{bmatrix}$$

∴ Since the above matrix is symmetric.

∴ the sum of the values at any column is 0.

Therefore, Calculated stiffness matrix is
Correct.

③ Evaluate the element stiffness matrix for the triangular element as shown in fig. under plane strain condition. Assume, $E = 200 \text{ GPa}$, $\nu = 0.28$ $t = 1 \text{ mm}$.



Sol:

$$A = 15 \text{ mm}^2 \quad t = 1$$

$$[B] = \frac{1}{30} \begin{bmatrix} -5 & 0 & 5 & 0 & 0 & 0 \\ 0 & -3 & 0 & -3 & 0 & 6 \\ -3 & -5 & -3 & 5 & 6 & 0 \end{bmatrix}$$

$$[D] = 8 \times 10^4 \begin{bmatrix} 3 & 1 & 0 \\ 1 & 3 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$$K = 1.33 \times 10^3$$

$$\begin{bmatrix} 84 & 30 & -16 & 0 & -18 & -30 \\ 30 & 52 & 0 & 2 & -30 & -54 \\ -16 & 0 & 84 & -30 & -18 & 30 \\ 0 & 2 & -30 & 52 & 30 & -54 \\ -18 & -30 & -18 & 30 & 36 & 0 \\ -30 & -54 & 30 & -54 & 0 & 108 \end{bmatrix}$$

Ans.

④ For the plane stress element, the nodal displacements are,

$$u_1 = 2 \text{ mm} \quad v_1 = 1 \text{ mm}$$

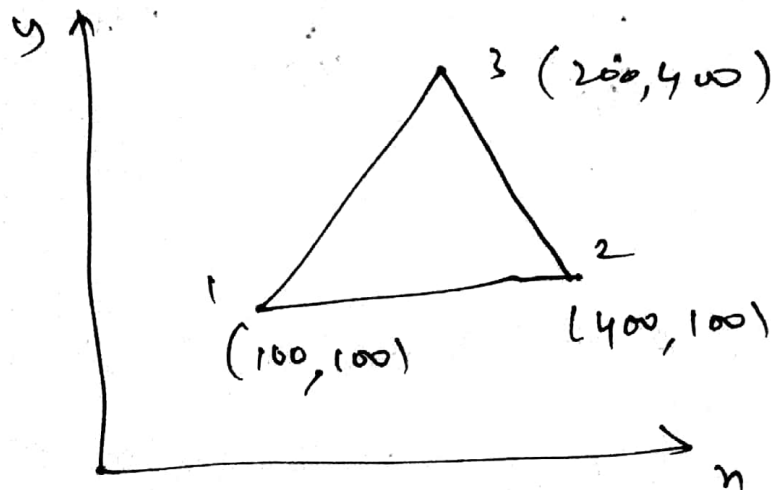
$$u_2 = 1 \text{ mm} \quad v_2 = 1.5 \text{ mm}$$

$$u_3 = 2.5 \text{ mm} \quad v_3 = 0.5 \text{ mm}$$

Determine the element stresses. Assume

$$E = 200 \text{ GPa/m}^2 \quad \nu = 0.3 \quad t = 10 \text{ mm}$$

all dimensions are in mm.



Sol:

$$[\sigma] = [D] \{e\}$$

$$[\sigma] = [D] [B] \{d\}$$

$$x_1 = 100$$

$$y_1 = 100$$

$$x_2 = 400$$

$$y_2 = 100$$

$$x_3 = 200$$

$$y_3 = 400$$

For plane stress,

$$[D] = \frac{E}{1-\mu^2} \begin{bmatrix} 1 & \mu & 0 \\ \mu & 1 & 0 \\ 0 & 0 & \frac{1-\mu}{2} \end{bmatrix}$$

$$= \frac{2 \times 10^5}{1-0.3^2} \begin{bmatrix} 1 & 0.3 & 0 \\ 0.3 & 1 & 0 \\ 0 & 0 & \frac{1-0.3}{2} \end{bmatrix}$$

$$[D] = \frac{2 \times 10^6}{91} \begin{bmatrix} 10 & 3 & 0 \\ 3 & 10 & 0 \\ 0 & 0 & 3.5 \end{bmatrix}$$

$$[B] = \frac{1}{2A} \begin{bmatrix} \beta_1 & 0 & \beta_2 & 0 & \beta_3 & 0 \\ 0 & \gamma_1 & 0 & \gamma_2 & 0 & \gamma_3 \\ \gamma_1 & \beta_1 & \gamma_2 & \beta_2 & \gamma_3 & \beta_3 \end{bmatrix}$$

$$\beta_1 = y_2 - y_3 = 100 - 400 = -300$$

$$\beta_2 = y_3 - y_1 = 400 - 100 = 300$$

$$\beta_3 = y_1 - y_2 = 100 - 100 = 0$$

$$\gamma_1 = x_3 - x_2 = 200 - 400 = -200$$

$$\gamma_2 = x_1 - x_3 = 100 - 200 = -100$$

$$\gamma_3 = x_2 - x_1 = 400 - 100 = 300$$

$$[A] = \frac{1}{2} \begin{vmatrix} 1 & x_1 & y_1 \\ 1 & x_2 & y_2 \\ 1 & x_3 & y_3 \end{vmatrix} = \frac{1}{2} \begin{vmatrix} 1 & 100 & 100 \\ 1 & 400 & 100 \\ 1 & 200 & 400 \end{vmatrix}$$

$$A = 45000 \text{ mm}^2.$$

$$[B] = \frac{1}{2 \times 45000} \begin{bmatrix} -300 & 0 & 300 & 0 & 0 & 0 \\ 0 & -200 & 0 & -100 & 0 & 300 \\ -200 & -300 & -100 & 300 & 300 & 0 \end{bmatrix}$$

$$[B] = \frac{1}{900} \begin{bmatrix} -3 & 0 & 3 & 0 & 0 & 0 \\ 0 & -2 & 0 & -1 & 0 & 3 \\ -2 & -3 & -1 & 3 & 3 & 0 \end{bmatrix}$$

$$f = \begin{bmatrix} u_1 \\ v_1 \\ u_2 \\ v_2 \\ u_3 \\ v_3 \end{bmatrix} = \begin{bmatrix} 2 \\ 1 \\ 1 \\ 1.5 \\ 2.5 \\ 0.5 \end{bmatrix}$$

$$\begin{bmatrix} F_{x1} \\ F_{y1} \\ F_{x2} \\ F_{y2} \\ F_{x3} \\ F_{y3} \end{bmatrix} = \frac{2 \times 10^6}{91} \begin{bmatrix} 10 & 3 & 0 \\ 3 & 10 & 0 \\ 0 & 0 & 3.5 \end{bmatrix} \frac{1}{900} \begin{bmatrix} -3 & 0 & 3 & 0 & 0 & 0 \\ 0 & -2 & 0 & -1 & 0 & 3 \\ -2 & -3 & -1 & 3 & 3 & 0 \end{bmatrix} \begin{bmatrix} 2 \\ 1 \\ 1 \\ 1.5 \\ 2.5 \\ 0.5 \end{bmatrix}$$

$$= \frac{2 \times 10^6}{91 \times 900} \begin{bmatrix} 10 & 3 & 0 \\ 3 & 10 & 0 \\ 0 & 0 & 3.5 \end{bmatrix} \begin{bmatrix} -3 \\ -2 \\ 4 \end{bmatrix}$$

$$\begin{bmatrix} \sigma_x \\ \sigma_y \\ \tau_{xy} \end{bmatrix} = \frac{2 \times 10^4}{819} \begin{bmatrix} -36 \\ -29 \\ 14 \end{bmatrix} = \begin{bmatrix} -879.12 \\ -708.18 \\ 341.88 \end{bmatrix} \text{ N/mm}^2$$

Maximum normal stress

$$\begin{aligned} \sigma_1 &= \frac{1}{2} \left[(\sigma_x + \sigma_y) + \sqrt{(\sigma_x - \sigma_y)^2 + 4\tau_{xy}^2} \right] \\ &= \frac{1}{2} \left[(-879.12 - 708.18) + \sqrt{(-879.12 + 708.18)^2 + 4(341.88)^2} \right] \\ &= \frac{1}{2} \left[-1587.3 + 704.81 \right] \\ \sigma_1 &= -441.24 \text{ N/mm}^2 \end{aligned}$$

Minimum normal stress

$$\begin{aligned} \sigma_2 &= \frac{1}{2} \left[(\sigma_x + \sigma_y) - \sqrt{(\sigma_x - \sigma_y)^2 + 4\tau_{xy}^2} \right] \\ &= \frac{1}{2} \left[-1587.3 - 704.81 \right] \\ \sigma_2 &= -1146 \text{ N/mm}^2 \end{aligned}$$

principle angle $\theta = \frac{1}{2} \tan^{-1} \left(\frac{2\tau_{xy}}{\sigma_x - \sigma_y} \right)$

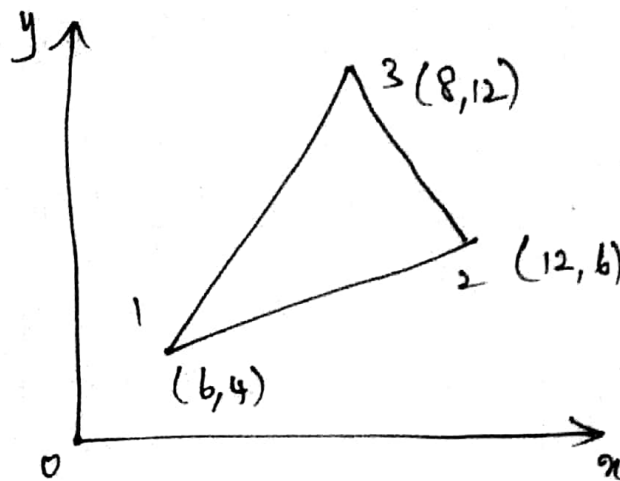
$$= \frac{1}{2} \tan^{-1} \left(\frac{2 \times 341.88}{-879.12 + 708.18} \right) = \underline{\underline{-37.98^\circ}}$$

5) The element shown in fig is subjected to a temperature change 10°C . Find the load due to temperature change.

Take $E = 200 \text{ GPa}$, $\mu = 0.3$, $t = 2 \text{ mm}$

$\alpha = 7 \times 10^{-6} / ^\circ\text{C}$. Assume plane stress conditions.

The coordinates in mm.



Sol:

$$x_1 = 6 \quad y_1 = 4$$

$$x_2 = 12 \quad y_2 = 6$$

$$x_3 = 8 \quad y_3 = 12$$

$$\Delta T = 10^\circ\text{C}$$

$$\alpha = 7 \times 10^{-6} / ^\circ\text{C} \quad \mu = 0.3 \quad t = 2 \text{ mm}$$

$$E = 200 \text{ GPa} = 200 \times 10^3 \text{ N/mm}^2 = 2 \times 10^5 \text{ N/mm}^2$$

$$[F_0] = [B]^T [D] [e_0] A t$$

↳ Thermal load Vector.

$$[B] = \frac{1}{2A} \begin{bmatrix} \beta_1 & 0 & \beta_2 & 0 & \beta_3 & 0 \\ 0 & \varrho_1 & 0 & \varrho_2 & 0 & \varrho_3 \\ \varrho_1 & \beta_1 & \varrho_2 & \beta_2 & \varrho_3 & \beta_3 \end{bmatrix}$$

$$A = \frac{1}{2} \begin{vmatrix} 1 & x_1 & y_1 \\ 1 & x_2 & y_2 \\ 1 & x_3 & y_3 \end{vmatrix} = \frac{1}{2} \begin{vmatrix} 1 & 6 & 4 \\ 1 & 12 & 6 \\ 1 & 8 & 12 \end{vmatrix}$$

$$A = 22 \text{ mm}^2$$

$$\beta_1 = y_2 - y_3 = 6 - 12 = -6$$

$$\beta_2 = y_3 - y_1 = 12 - 4 = 8$$

$$\beta_3 = y_1 - y_2 = 4 - 6 = -2$$

$$\varrho_1 = x_3 - x_2 = 8 - 12 = -4$$

$$\varrho_2 = x_1 - x_3 = 6 - 8 = -2$$

$$\varrho_3 = x_2 - x_1 = 12 - 6 = 6$$

$$[B] = \frac{1}{44} \begin{bmatrix} -6 & 0 & 8 & 0 & -2 & 0 \\ 0 & -4 & 0 & -2 & 0 & 6 \\ -4 & -6 & -2 & 8 & 6 & -2 \end{bmatrix}$$

$$[B]^T = \frac{1}{44} \begin{bmatrix} -6 & 0 & -4 \\ 0 & -4 & -6 \\ 8 & 0 & -2 \\ 0 & -2 & 8 \\ -2 & 0 & 6 \\ 0 & 6 & -2 \end{bmatrix}$$

For plane stress,

$$D = \frac{E}{1-\mu^2} \begin{bmatrix} 1 & \mu & 0 \\ \mu & 1 & 0 \\ 0 & 0 & \frac{1-\mu}{2} \end{bmatrix}$$

$$= \frac{2 \times 10^5}{1-0.3^2} \begin{bmatrix} 1 & 0.3 & 0 \\ 0.3 & 1 & 0 \\ 0 & 0 & \frac{1-0.3}{2} \end{bmatrix}$$

$$[D] = \frac{2 \times 10^6}{91} \begin{bmatrix} 10 & 3 & 0 \\ 3 & 10 & 0 \\ 0 & 0 & 3.5 \end{bmatrix}$$

$$e_0 = \begin{bmatrix} \alpha \Delta T \\ \alpha \Delta T \\ 0 \end{bmatrix} = \begin{bmatrix} 7 \times 10^{-5} \\ 7 \times 10^{-5} \\ 0 \end{bmatrix}$$

$$\therefore [F_0] = [B]^T [D] [e_0] A t$$

$$\begin{bmatrix} F_{1x} \\ F_{1y} \\ F_{2x} \\ F_{2y} \\ F_{3x} \\ F_{3y} \end{bmatrix} = \frac{1}{44} \begin{bmatrix} -6 & 0 & -4 \\ 0 & -4 & -6 \\ 8 & 0 & -2 \\ 0 & -2 & 8 \\ -2 & 0 & 6 \\ 0 & 6 & -2 \end{bmatrix} \frac{2 \times 10^6}{91} \begin{bmatrix} 10 & 3 & 0 \\ 3 & 10 & 0 \\ 0 & 0 & 3.5 \end{bmatrix} \begin{bmatrix} 7 \times 10^{-5} \\ 7 \times 10^{-5} \\ 0 \end{bmatrix} \quad (22 \times 2)$$

$$= \frac{2 \times 10^6 \times 22 \times 2}{94 \times 91} \begin{bmatrix} -60 & -18 & -14 \\ -12 & -40 & -21 \\ 80 & 24 & -7 \\ -6 & -20 & 28 \\ -20 & -6 & 21 \\ 18 & 60 & -7 \end{bmatrix} \begin{bmatrix} 7 \times 10^{-5} \\ 7 \times 10^{-5} \\ 0 \end{bmatrix}$$

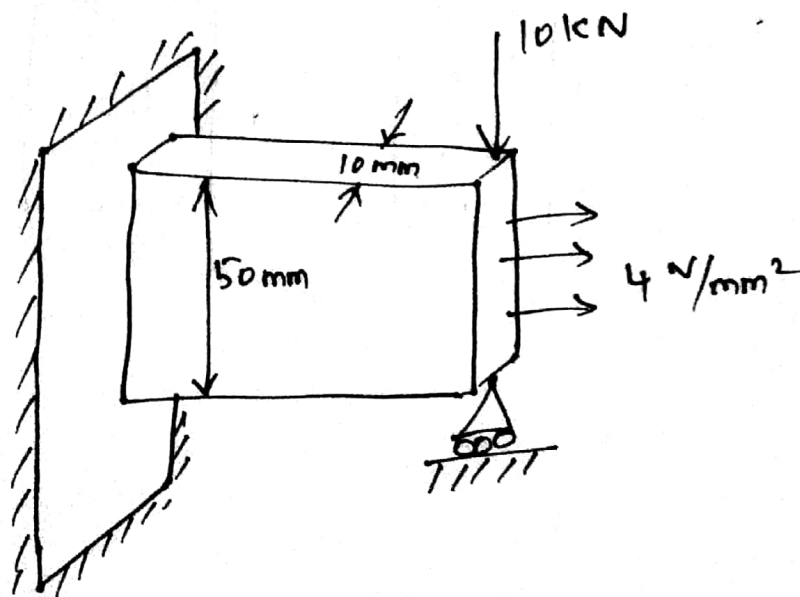
$$= \frac{2 \times 10^6}{91} \times 7 \times 10^{-5} \begin{bmatrix} -60 & -18 & -14 \\ -12 & -40 & -21 \\ 80 & 24 & -7 \\ -6 & -20 & 28 \\ -20 & -6 & 21 \\ 18 & 60 & -7 \end{bmatrix} \begin{bmatrix} 1 \\ 1 \\ 0 \end{bmatrix}$$

$$= \frac{140}{91} \begin{bmatrix} -78 \\ -52 \\ 104 \\ -26 \\ -26 \\ 78 \end{bmatrix} = \begin{bmatrix} -120 \\ -80 \\ 60 \\ -40 \\ -40 \\ 120 \end{bmatrix} N$$

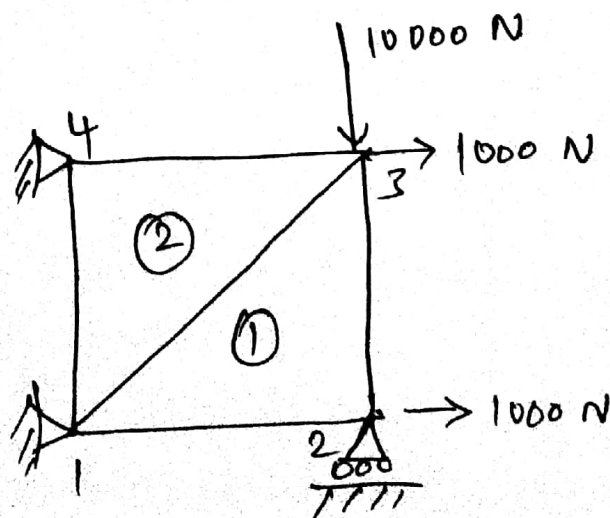
University Problem :

For a thin plate subjected to the surface traction force along with an external load as shown in fig. determine the nodal displacements and element stresses.

Thickness $t = 10 \text{ mm}$ $E = 210 \text{ GPa}$ $\nu = 0.25$. Analyse the plate using two element model.



Sol:



$$\text{Nodal Force} = \frac{1}{2} TA.$$

$T \rightarrow$ Traction force. ($\frac{N}{mm^2}$)

$$F = \frac{1}{2} \times 4 \times (50 \times 10)$$

$$F = 1000 N. \text{ @ node 2 \& 3.}$$